

# **Pole Top Structure Replacements** Business Case

18 November 2024



# **CONTENTS**



## **REFERENCED DOCUMENTS**



# <span id="page-3-0"></span>**1 SUMMARY**







# <span id="page-6-0"></span>**2 PURPOSE AND SCOPE**

The purpose of this business case is to outline the drivers for the proposed replacement and expenditure associated with the pole top structure replacement program for the 2025-30 regulatory period. This business case covers only the defect-based and targeted replacements of pole top structures. Consequential replacement expenditure is included in their respective business cases. The document includes the analysis of different options to address this need to demonstrate prudency through NPV modelling.

This document is to be read in conjunction with the Repex Ex-Post and Ex-Ante Narrative attachment 5.5.01A.

All dollar values in this document are based upon real 2024/25 dollars and exclude overheads.

## <span id="page-7-0"></span>**3 ASSET PORTFOLIO**

## <span id="page-7-1"></span>**3.1 Asset Population**

Ergon Energy's Network pole top structure of 1.2 million includes 1.15 million timber pole top structures with most of the remaining population being composite, as detailed in [Figure 1.](#page-7-2) The age of pole top structures is inferred from the age of poles Our age profile of timber pole top structures shows that over 43% are operating beyond expected useful life, including over 500,000 older than 35 years old or their useful life.

Composite pole top structures were introduced from late 2000s and since then volumes have been increasing steadily. This increased uptake of composite pole top structures will provide significant benefits for asset longevity, electricity performance, and are more lightweight. They also deform or bend rather than break when conductors are damaged, which lowers their safety risk.

Timber pole top structures are susceptible to several life limiting factors including environmental stress such as high rainfall and extreme heat, termite and rotting impacts and splitting and a transition to composite pole top structures will minimise these impacts.

<span id="page-7-2"></span>

#### **Figure 1 : Pole Top Structure Age Profile**

## <span id="page-8-0"></span>**3.2 Historical Asset Performance**

[Table 1](#page-8-1) presents the two main functional failures of pole top structures.

<span id="page-8-1"></span>



[Figure 2](#page-8-2) displays the number of unassisted pole top structure failures. All these failures are from wood pole top structures as there have been no reports of composite or steel pole top structure unassisted failures.

<span id="page-8-2"></span>The main causes of failure are rot and decay, which make up 75% of failures. This unassisted failure data indicates a steady trend in recent three years, averaging around 300 failures per year.



#### **Figure 2 : Pole Top Structure Unassisted Failures**

Identified defects are scheduled for repair according to a risk-based priority scheme (P0/P1/P2/C3/no defect). The P0, P1, and P2 defect categories relate to the priority of repair, which effectively dictates whether normal planning processes are employed (P2), or more urgent repair works are initiated (P1 and P0). C3 defects are identified from ground and aerial based inspections and are defined as minor deterioration or damage which requires no specific action or does not indicate an acceptable likelihood of failure or creation of a hazardous event in the medium term. This type of defect is the final step before the defect is classified as a P1 or P2 defect which means Ergon Energy has a responsibility to rectify within prescribed period.

[Figure 3](#page-9-1) contains the volume of pole top structure which have been identified as having P1 and P2 defects. The defect data indicates over 13,000 defects in 2018-19 followed by consistently high volumes averaging approximately 9,600 defects per year over the four subsequent years. The variation in defect volumes can be attributed to various interventional programs including proactive replacements, reconductoring, pole replacement, clearance to ground (CTG), clearance to structure (CTS), and the aerial inspection program.

<span id="page-9-1"></span>

#### **Figure 3 : Pole Top Structure Defects**

#### <span id="page-9-0"></span>**3.3 Asset Management**

Pole top structure replacements are mostly driven by well-established inspection programs which identify severe structural strength degradation. Once identified, defects are addressed in a planned manner, aligned with defect policy time frames, to manage asset conditions. This approach helps mitigate risks and reduce the likelihood of unexpected failures by addressing potential issues before they escalate.

Ergon Energy's asset management practices include:

- Visual inspection of physical condition from ground level at approximately 270,000 sites per year on a 5-year compliance cycle;
- Aerial visual inspection carried out from helicopters/aircraft/drones at approximately 36,000 sites per year according to criteria; and
- Pole top structures inspection carried out from an elevated work platform or by climbing at approximately 6,000 sites per year on a 4- or 5-year cycle.

Physically defective pole top structures identified through inspection are replaced. They may also be proactively replaced based on risk assessment. Proactive replacement is typically undertaken with other work such as feeder refurbishment programs or bundled into logical groups for efficiency of delivery and cost. Safety risks associated with pole top structures aim to be eliminated so far as is reasonably practicable (SFAIRP) or mitigated SFAIRP. All other risks are managed as low as reasonably practicable (ALARP).

The current strategy is to transition away from timber pole top structures in favour of alternatives, such as composite pole top structures as composite pole top structures have a much longer lifespan and a lower safety risk. Since 2010, Ergon Energy predominately using composite material where possible.

We have also recently improved the quality of the collected field, population, and failure data for our pole top structure population. The improved data captured has indicated a flat rate in the past three years for unassisted pole top structure failures.

The statistical Weibull model is used for assets that only have inspection data, and no measured data to derive the Probability of Failure (PoF).

## <span id="page-10-0"></span>**3.4 Compliance**

Ergon Energy's pole top structure assets are subject to several legislative and regulatory standards. This includes:

- The Electrical Safety Act 2002 (Qld) s29 imposes a specific duty of care on a prescribed Electrical Entity to ensure that its works are electrically safe; and operated in an electrically safe way. The duty includes the requirement that the electricity entity inspects, tests and maintains the assets and works.
- The Electrical Safety Regulation 2013:
	- $\circ$  details requirements for electric lines, specifically about safety clearances, of which pole top structures are classed as associated equipment. These include various general obligations related to the safety of works of an electrical entity.
	- $\circ$  The desired level of service for pole top structures in the Ergon Energy network is to achieve in-service pole top structure failure numbers which deliver a safety risk outcome which is considered SFAIRP.

## <span id="page-11-0"></span>**4 PROBLEM STATEMENT**

Ergon Energy's current strategy for pole top structure replacements is driven by well-established inspection programs to identify observed structural degradation. Replacements of pole top structures are actively managed through a condition-based approach.

However, the current strategy has not delivered the desired level of improvements to our service levels which our customers expect and require.

Due to our concerns with the risk of an ageing population and emerging C3 defective volumes, as well as to ensure the improvement of asset performance, we consider it important to introduce a step-change in our replacement strategy that includes a proactive and targeted replacement approach for this asset group. This will help us ensure our service levels for customers are improved.

#### • **Pole top structure performance has not improved**

Pole top structure risks are regularly assessed through asset inspection and defect identification processes. Our most recent analysis has revealed that unassisted failures continue to be trending upwards as shown in [Figure 2.](#page-8-2)

#### • **Defective pole top structure presents a significant safety risk**

Currently, our pole top structure assets are ageing, presenting a growing safety risk. More than 30% of our pole top structures are operating beyond their expected useful life, increasing the risk of failure. This is a significant concern as an average of around 20% of pole top structure failures lead to a conductor falling to the ground, exposing a high safety risk to the community.

#### • **Growing number of C3 defects**

Our current approach is to replace the inspection-driven defective pole top structures, which is approximately 9,000 replacements per annum. However, in addition to this, we have approximately 80,000 pole top structures that have been identified as emerging C3 defects or having minor deterioration over the last 3 years. A few of these C3 defective assets will be addressed consequentially during pole and conductor replacements, at a volume similar to defect replacements, however the remaining C3 defects still present a growing risk to the network.

## <span id="page-12-0"></span>**5 BENEFIT AND RISK ANALYSIS**

### <span id="page-12-1"></span>**5.1 Overview**

Following feedback from the AER on the CBA modelling used, we have revised our CBA and details are in Appendix B – [Revised modelling approach.](#page-29-0) Our cost-benefit analysis aims to optimise our risk calculation at the program level, so that on average we will be able to maximise the benefits to our customers.

After conducting a cost-benefit analysis using net present value (NPV) modelling, the most positive NPV of the volumes considered will form the basis for selecting the preferred option. In the NPV modelling, the monetised risk is calculated by as per the calculation in [Figure 4.](#page-12-2)

<span id="page-12-2"></span>

Ergon Energy broadly considers five risk streams for investment justifications for the replacement of widespread assets. These are shown in [Figure 5.](#page-12-3)

<span id="page-12-3"></span>

#### **Figure 5 : Benefit and Risk Stream for Assets**

## <span id="page-13-0"></span>**5.2 Probability of Failure**

Typically, Ergon Energy uses an Asset Health Index (HI) to assess the probability of failure of an asset. However, due to the limited condition data available for pole top structures, the Weibull distribution model is used instead. The Weibull distribution is widely used due to its flexibility and ability to model skewed data. Its ability to work with an extremely small number of sample (less than 20 samples) makes it the best choice, if not the best practice.

It is a versatile distribution that can take on the characteristics of other types of distributions, based on the value of the shape parameter, beta (β) and the scale parameter, eta (η). Shape parameter eta defines the average period when 63.2% of asset population is expected to fail. The other parameter represents the failure rate behaviour, if beta is less than 1, then the failure rate decreases with time; if beta is greater than 1, then the failure rate increases with time. When beta is equal to 1, the failure rate is constant.

The function used to determine the probability of failure from a particular asset's age is the Cumulative Distribution Function (CDF). By modelling historical pole top structure failures and age at the time of failure, a Weibull curve can be derived which can then be used to estimate the probability of failure (PoF) for each age group.

[Figure 6](#page-13-1) shows the Weibull cumulative distribution function for pole top structures.

<span id="page-13-1"></span>

#### **Figure 6 : Pole top structure failure plot against Weibull CDF Curve**

<span id="page-14-1"></span>The resulting Weibull parameters are outlined in [Table 2.](#page-14-1)

#### **Table 2 : CDF Weibull Variables**



## <span id="page-14-0"></span>**5.3 Consequence of Failure (CoF) and Likelihood of Consequence (LoC)**

The consequence categories that have been modelled are reliability, financial, safety and environmental. The CoF refers to the economic outcomes if a failure event (such as a bushfire) were to occur.

The LoC refers to the probability of a particular result (e.g. an outage or fatality) occurring because of a failure event (e.g. ageing of the asset). To estimate the LoC, Ergon Energy has used a combination of historical performances and researched results. Ergon Energy has analysed past events, incidents, and data to identify patterns and trends that can provide insights into the likelihood of similar outcomes occurring in the future. Additionally, Ergon Energy also has conducted extensive research to gather relevant information and data related to the respective risk category.

To the extent possible, the identified CoF and LoC are pole top structure age-band specific. This is particularly the case for the reliability and benefits stream, where the site-specific location and bushfire risk informs the benefits calculations for preventing unassisted pole top structure failures.

#### **5.3.1 Reliability**

Reliability represents the unserved energy cost to customers impacted by network outages and is based on an assessment of the amount of Load at Risk during three stages of failure: fault, initial switching, and repair time. The following assumptions are used in developing the risk cost outcome for a pole top structure failure:

- **Lost load:** Each pole top structure in our network is modelled individually, with the relationship developed between a pole top structure and the pole and feeder/conductor that it is supporting. The historical average load on each feeder in our network is used to determine the kilowatt (kW) that would on average be lost following a pole top structure failure. We have used half of the historic average load on the feeder, which represents the most likely outcome. This is because a pole top structure is not a uniquely identified asset and therefore the data regarding the exact electrical location of the pole top structure in a feeder is not feasible to obtain.
- **Load transfers and Restoration time frame:** The average loss of supply has been estimated for a period of average 4 to 9 hours based on locality, staged restoration

approach, and historical data for outages/durations. This is based on the average load on our fleet of feeders, divided under rural short, rural long, urban, and sub-transmission.

- **Value of Customer Reliability Rate:** We have used the Queensland average Value of Customer Reliability (VCR) rate.
- **Probability of Consequence:** For modelling purposes, any pole top structure failure that results in a conductor drop has been assumed to cause an outage to customers.

#### **5.3.2 Financial**

The financial cost of failure is derived from an assessment of the likely replacement costs incurred by the failure of an asset that is replaced under emergency. The same unit cost has been taken for replacement in both planned and unplanned circumstances. Historical average cost has been used for this purpose and is approximately \$2,800.

#### **5.3.3 Safety**

The primary safety risk for a pole top structure failure is that a member of the public could be in the presence of a fallen conductor which was caused by pole top structure failure. This could result in a fatality or injury. For our modelling, we have used the Best Practice Regulation Guidance Note<sup>1</sup> from the Australia Government Department of Prime Minister and Cabinet with the following assumptions:

- **Value of a Statistical Life:** \$5.4m
- **Value of an Injury:** \$1.35m
- **Disproportionality Factor:** 6 for members of the public and 3 for internal staff
- **Probability of Consequence:** Following an unassisted pole top structure failure, there is a 1 in 20-year chance of causing a fatality and 25 in 20-year chance of a serious injury based on historical data evidence.<sup>2</sup>

<sup>1</sup> August 2022 document from the Australian Government, Department of the Prime Minister and Cabinet (Office of Best Practice Regulation) Best Practice Regulation Guidance Note - Value of a Statistical Life

 $2$  The average number of safety incidents has been derived by analysing 20 years of significant electrical incident data comprising 26 incidents where unassisted asset failure has driven a safety incident of the appropriate severity. Historically, the data shows that pole top structure have not been the cause of fatality, therefore the fatality incident due to a conductor asset unassisted failure has instead been considered for modelling purpose.

#### **5.3.4 Environment (Bushfire)**

The value of a Bushfire Event consists of the safety cost of a fatalities and the material cost of property damage following a failed pole top structure and conductor. For our modelling, we have used:

- **Value of Bushfire:** \$22.3m which is the average damage to housing and fatalities following a bushfire starting.<sup>3</sup>
- **Safety Consequence of Bushfire:** Safety consequences are evaluated on the same assumptions as safety incident consequence with a frequency of 0.5 per incident as there has been 6 fatalities recorded across those 12 bushfire incidents in Queensland.
- **Probability of Consequence:** Following the failure of a pole top structure, we have estimated that there is a 0.0260 chance of causing a fire. This is based on a historical full year when there were 22 fires recorded due to electrical asset failures in Ergon Energy. In that year, there were 114 pole failures, 265 pole top structure failures and 467 conductor failures that had potential to cause fire ignition, giving a probability of 0.0260 (22/846).
	- $\circ$  Also, bushfire consequence weighting and probability of containing/non-containing the fire has been incorporated into calculations along with % number of days considerations during no-forecast to extreme/catastrophic danger rating forecasts. A fire is also only considered to be possible if the conductor has dropped and made contact with the ground due to the failure of a pole top structure. In 2021, a total of 56 conductors dropped in the 274 failures recorded. Therefore a 20.4% factor has been considered as part of the probability of consequence.

<sup>3</sup> Calculated using data from *Australian Major Natural Disasters.xlsx* (a compendium of various sources). The source shows that in Queensland there were 122 homes and 309 buildings lost during bushfires between 1990 and 2021 across 12 significant fire records. Homes were estimated at an average cost of \$400,000 while the buildings were estimated at an average cost of \$80,000

## <span id="page-17-0"></span>**6 COUNTERFACTUAL ANALYSIS**

Ergon Energy has taken the AER's Draft Decision feedback into consideration when developing the counterfactual option for this business case and has also taken into consideration the AER's Industry practice application note for asset replacement planning. In particular, the counterfactual option has been represented as the costs that consumers would incur if the asset continued to be operated under the standard operating and maintenance practices or, 'do nothing materially different' under its usual asset management practices.

The counterfactual considered in this business case is continuing with the existing strategy of replacing pole top structures based on historical defect average of 8,736 pole tops per annum. This is representative of the three-year actual defects averaged over the period 2020/21, 2021/22 and 2022/2023.

## <span id="page-17-1"></span>**6.1 Counterfactual Costs and Volumes**

The estimated volume and expenditure for the counterfactual option are shown in the tables below. [Table 4](#page-17-3) shows that, although the volume remains constant each year, the cost varies. This is due to the differing unit costs associated with each voltage category.



#### **Table 3 : Counterfactual Option – Volumes**

#### <span id="page-17-3"></span>**Table 4 : Counterfactual Option – Costs**



\*Variation in cost is due to the differing unit costs associated with each voltage category.

## <span id="page-17-2"></span>**6.2 Counterfactual Risk and Benefit Quantification**

Ergon Energy has determined the risk and benefits over a thirty-five-year time horizon as a period representative of the expected period of realisable benefits from any interventions. [Figure 7](#page-18-0) and [Figure 8](#page-18-1) provides the results of the counterfactual failure forecast and quantitative forecast of emerging risk associated with Ergon Energy pole top structure asset population failure. The risk increases substantially due to a large number of poor condition (end of service life) pole top structures over 35 years still being in service requiring intervention and posing safety and reliability risk to community.

<span id="page-18-0"></span>

**Figure 7 : Unassisted Failures Forecast: Counterfactual**



<span id="page-18-1"></span>

# <span id="page-19-0"></span>**7 OPTIONS AND ECONOMIC ANALYSIS**

## <span id="page-19-1"></span>**7.1 Overview of Options**

We have considered and compared a range of potential options against the counterfactual / business-as-usual approach and have sought to identify technically feasible, alternative options that satisfy the identified need and problem statement in a timely and efficient manner. The tables below provide an overview of the costs and volumes for each of the options considered.

The options that have been considered include:

- Option 1 replace only those pole top structures that have failed
- Option 2 replace those pole top structures that have been identified as defective as well as a low volume 3,500 (5% of C3) of targeted / proactive pole top structures that have been identified as a C3 emerging defect
- Option 3 replace those pole top structures that have been identified as defective as well as a 7,000 (10% of C3) targeted / proactive pole top structures that have been identified as a C3 emerging defect
- Option 4 replace 172,640 in 5 years estimated from CBA analysis has been deemed the optimal replacement volume.

**Option 4 – Optimal replacement**  ume



#### **Table 5 : Summary of Options costs and volumes**

#### **Table 6 : Costs for each option over 2025-30 period**



**Table 7 : Volumes for each option over 2025-30 period**



## <span id="page-20-0"></span>**7.2 NPV and Economic Analysis**

The pole top structure failure forecast for all options is shown in [Figure 9.](#page-21-0) In Option 1, where defects are left unattended, unassisted failures will escalate significantly to an unsustainable level. Option 2 and Option 3 (Preferred Option) are expected to produce better outcome than counterfactual, with Option 4 providing least failure rate among options considered but an expensive and delivery risk option.

<span id="page-21-0"></span>

**Figure 9 : Unassisted Failures Forecast: All Options**

The risk cost for each of the options considered are provided in [Table 8.](#page-21-1)



<span id="page-21-1"></span>**Table 8 : Total Risk Cost: All Options**

The NPV ranking and economic analysis is summarised in [Table 9](#page-22-0) which demonstrates that:

• Counterfactual option does not meet the identified need and problem

- Option 2, 3 and 4 demonstrate a positive NPV against the counterfactual, compared to Option 1 which provides a negative NPV
- Option 4 has the highest NPV to meet the identified need. However, it will require additional resourcing and presents deliverability concerns.
- **Option 3 is the preferred option** as it NPV positive, meets the identified need and has no deliverability risks. It also delivers a high benefit-to-cost ratio which indicates a substantial benefit over the costs. Whilst Option 2 is also NPV positive, it only addresses 5% of the identified C3 emerging defects and therefore does not fully address the identified need.

#### <span id="page-22-0"></span>**Table 9 : NPV Modelling and BCR Analysis Outcomes: All Options**



[Figure 10](#page-23-1) illustrates the NPV analysis of the options against the counterfactual.

<span id="page-23-1"></span>

#### **Figure 10 : NPV Analysis for Each Option Against Counterfactual**

# <span id="page-23-0"></span>**7.3 Assumptions and Variables**

[Table 10](#page-23-2) below presents the relevant assumptions and variables that were considered in undertaking the NPV and economic analysis.

<span id="page-23-2"></span>



## <span id="page-24-0"></span>**7.4 Validation of Modelled Risk Value**

As part of development of the revised CBA models, Ergon Energy undertook a model validation exercise using actual outage analysis. This data was collected for each unassisted pole failure:

- 1. For all the outages, the unserved energy to the customer was obtained, including the restoration time.
- 2. The VCR \$53.47/kWh value was derived from the weight average calculation based on the AER 2023 VCR publication.
- 3. Using the \$53.47/kWh, the reliability cost was calculated for each unassisted failure.
- 4. This reliability cost was then compared with the predictive model's reliability risk cost output.
- 5. In the FY2022-23, the outage reliability cost due to unassisted pole failures of \$11.6m is comparable with the year 1 predictive model output of \$14.9m. (attachment 5.5.01E)

## <span id="page-24-1"></span>**7.5 Sensitivity Analysis**

To further test the effectiveness and prudency of the preferred option, several sensitivity analysis criteria have been applied, with  $\pm 25\%$  values, to compare modelled outcomes in different scenarios. The main sensitivity criteria are:

- Weighted Average Capital Cost (WACC)
- Risk/Benefit

Option 4 – Optimum Replacement Volume (34528) has been demonstrated as the most prudent option.







#### **Table 12 : NPV Sensitivity Analysis with 25% Increased Base WACC (3.5%)**

#### **Table 13 : NPV Sensitivity Analysis with 25% Reduced Risk/Benefit**





#### **Table 14 : NPV Sensitivity Analysis with 25% Increased Risk/Benefit**

## <span id="page-27-0"></span>**8 RECOMMENDATION**

After a thorough evaluation of all available and feasible options, Option 3 is the optimum and most efficient option that addresses the identified need. This option has been chosen as it demonstrates that incorporating a proactive targeted replacement approach, along with the existing defect replacement strategy, provides the highest benefits to the customer and provides a positive net NPV of \$170 million over the modelling period. The targeted 7,000 per annum will focus on 10% of the already identified 80,000 C3 pole top structure defects that are primarily located in coastal regions of the Ergon Energy network, where there is generally a higher level of rainfall and therefore a higher proportion of pole top structure deterioration.

Furthermore, we will continue to focus on optimising existing processes and enhancing efficiencies where possible to deliver additional benefits through consequential replacements of pole top structures in other programs.

Option 3 reflects a tolerable risk position which balances the achievement of asset management objectives and customer service levels and ensures a level of investment which avoids future consequences based on the uncertainty associated with the capability new technologies may bring.

## **APPENDIX A – OPTIONS COMPARISON**

The analysis presented in [Table 15](#page-28-1) compares the options to the respective counterfactual alternative.

#### <span id="page-28-1"></span>**Table 15 : Comparison of options considered**

<span id="page-28-0"></span>

# <span id="page-29-0"></span>**APPENDIX B – REVISED MODELLING APPROACH**

Following feedback from the AER on the CBA modelling used for the Regulatory Proposal and the feedback from our workshops with the AER, we have modified our modelling approach for the Revised Regulatory Proposal. Due to the step change of replacements proposed for pole top structures, this is considered an ex-ante forecast. [Table 16](#page-29-1) provides the outputs as a result of this change.

<span id="page-29-1"></span>**Table 16: Differences in model outputs for pole top structures between the Regulatory Proposal and Revised Regulatory Proposal**



## <span id="page-30-0"></span>**9 GLOSSARY**

